

# Modification of Varying Load Creep Testing Machine to find Creep Behaviour of Lead Material

Arvind Totey and Dr. Hardik Bhupendrabhai Ramani

Department of Mechanical Engineering,  
Dr. A.P.J. Abdul Kalam University, Indore (M.P.) - 452010

## Abstract

This paper covers the design analysis and fabrication of a tensile creep test machine for determining the creep behaviour curve for thermoplastic materials like polypropylene and light metals like lead. The purpose of the work was to fabricate a machine at low cost and may be used in college laboratory to demonstrate creep behaviour curve. The lever mechanism of conventional machine is replaced by a connecting mild steel metalwire. The load is applied with the help of turn buckle of 22500N. Different capacities of tension spring are used to vary loads. The tension spring of 39.24N, 245.25N and 392N is used. A low heat treatment furnace of capacity below 200°C is designed. The temperature is indicated on PID temperature controller.

**Keywords:** Thermoplastic, Turnbuckle, Tension spring, Creep test, design, mild steel, furnace, lead.

**Objectives of Project:** The objective of this work is to design and fabricate a Creep test apparatus which can be used in laboratory to demonstrate creep behaviour of engineering materials without using expensive creep testing machine.

## 1. Introduction

A creep-testing machine measures the creep (the tendency of a material after being subjected to high levels of stress, e.g. high temperatures, to change its form in relation to time) of an object. It is a device that measures the alteration of a material after it has been put through different forms of stress. Creep machines are important to see how much strain (load) an object can handle under pressure, so engineers and researchers are able to determine what materials to use. The device generates a creep time-dependent curve by calculating the steady rate of creep in reference to the time it takes for the material to change. Creep machines are primarily used by engineers to determine the stability of a material and its behaviour when it is put through ordinary stresses.

The first creep testing machines were created in 1948 in Britain to test materials for aircraft to see how they would stand in high altitudes, temperature and pressure. The machines were first developed to further calculate and understand the steady rate of creep in materials. Creep is the tendency of a material to change form over time after facing high temperature and stress. Creep increases with temperature and it is more common when a material is exposed to high temperatures for a long time or at the melting point of the material. Creep machines are used to understand the creep of materials and determine which type can do the job better, which is important when making and designing materials for everyday uses. They most commonly test the creep of alloys and plastics for the understanding of their properties and advantages of one material's use over another. Different stages of creep are shown in fig no 1.

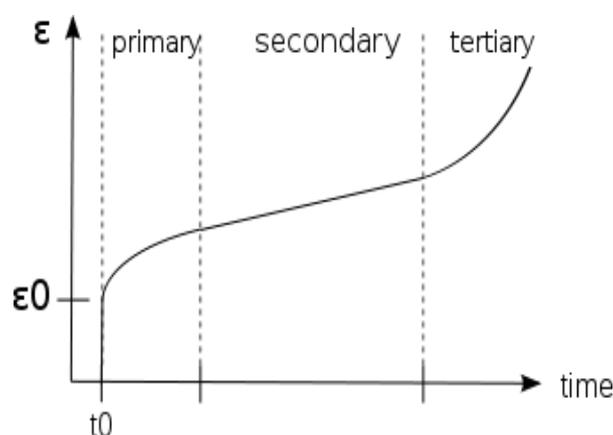


Figure 1: stages of creep

## 2. Methodology

### 2.1 Design of Machine Components

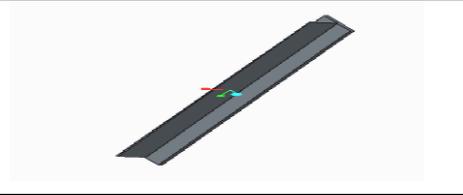
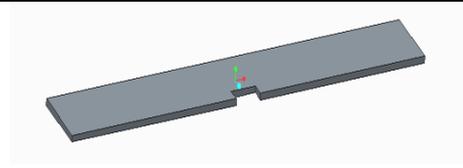
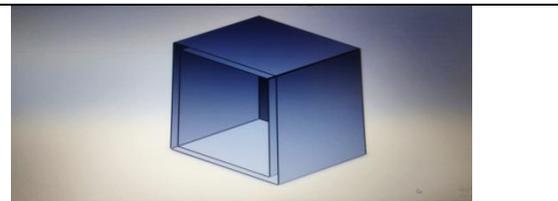
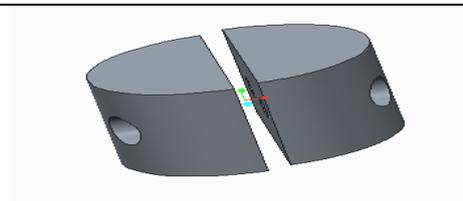
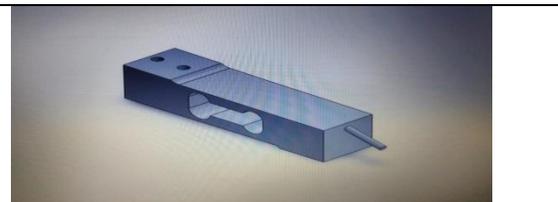
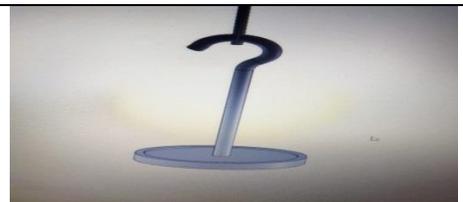
Machine Components Parts	
Components of Creep Testing Machine	
1. Base part	2. Column
	
3. Column Support Plate	4. Rectangular Top Plate
	
5. Extended Top angle	6. Bracket for Load Cell
	
7. Heating Chamber	8. Test piece grip
	
9. Load cell	10. Load hanger
	
11. Turnbuckle	12. Tension helical spring
	

Table 1: Machine Components Parts

### 3. Test Specimens

Test specimens for Tensile Creep Testing Machine used are lead. The standard test specimen should be in the form of "I" Section

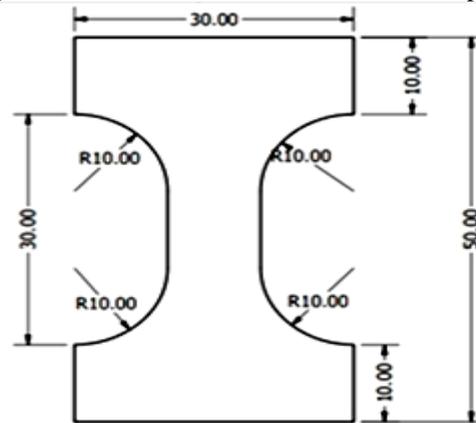


Figure 2: Test Specimens Geometry

### 4. Design Calculations for Furnace

The components of the furnace are as follows:

The Heating element, Outer Casing, Insulating Materials, Grippers, Digital Temperature Indicator

The dimensions of the furnace are assumed as follows:-

Outer Length = 152mm Outer Breadth = 128mm Outer Height = 224 mm Inner Length = 124 mm Inner Breadth = 115mm Inner Height = 200mm

The furnace is designed for maximum temperature up to 200° C and the outer surface temperature is assumed to be 30° C. for testing the specimen is fixed in the grippers in furnace which are used to hold the specimen in testing period. The lower gripper is fixed and the upper gripper is movable.

After fixing the test specimen, desired load is applied via turn buckle. When the desired load is achieved, required temperature is set inside the furnace by the help of digital temperature controller. Due to applied temperature and load after some time duration, creep phenomena are generated in the test specimen and elongation of length is produced as a result.

Taking properties at the required temperatures from data book such as density ( $\rho$ ), specific heat ( $C_p$ ), thermal conductivity ( $k$ ), kinematic viscosity ( $\nu$ ), and number ( $Pr$ ).

At  $T_o=30^\circ C$ .

$Gr_L=241.62 \times 10^6$  (at  $x=L=224mm$ )  $Gr_L \cdot Pr = 169.37 \times 10^6$ . Calculating Nusselt no,  $Nu=0.59 \times (Gr_L \cdot Pr)^{0.25}$   $Nu=67.30$   $Nu=\frac{h_o \cdot L}{k}$ ,  $h_o=9.00$  w/m-K similarly, at  $T_i=200^\circ C$   $Gr_L=23.17 \times 10^6$   $Gr_L \cdot Pr=15.76 \times 10^6$   $Nu=37.17$ ,  $h_i=7.30$  w/m-k

Calculating heat dissipated through wall of the furnace, Where  $A_1=0.124m^2$   $A_2=0.15m^2$   $A_3=0.164m^2$   $K=0.087$  (from data book for bison sheet)  $Q_w=60$  watt, Calculating heat dissipated through grippers, selecting cast steel as a material for gripper as it can sustain the required temperature, Volume= $\pi r^2 \cdot h$  Where  $r=35 \times 10^{-3}m$   $h=70 \times 10^{-3}m$ , Volume= $2.69 \times 10^{-4}m^3$  · Density= $7753$  kg/m<sup>3</sup>, Specific heat= $486$  J/kg-K  $Q_g=mC_p \Delta T$ , Assuming  $t=15$  minutes,  $M=2.31 \times 10^{-3}$ ,  $Q_g=191.45$  watt. The specimen to tested is in the form of I section.

Therefore, selecting Teflon as the material for specimen as its creep temperature is  $130.72^\circ C$ . which is in the range.

Adding all the heat dissipated  $Q_T=252.25$  watt, this energy is absorbed by the elements of the Furnace; hence we have to consider heating coil having wattage close to the obtained result.

### 5. Design of Turnbuckle

**Step 1:-** Selection of Material for turnbuckle, Stainless steel  $S_{ut} = 465$  MPa,  $S_{yt} = 270$  MPa

**Step 2:-** Selecting M8 designated Turnbuckle for Max load application,  $d = 8mm$ ,  $d_c = 6.466$  mm,  $P = 400N$

Tensile Stress  $\sigma_t = 12.18$  N/mm<sup>2</sup> Torsional moment  $M_t = 313.6$  N-mm shear stress,  $\tau = 5.91$  N/mm<sup>2</sup>

The principle shear stress is given by,  $\tau_{max} = 8.486$  N/mm<sup>2</sup> Factor of safety,  $f_s = 15.90$

The factor of safety is satisfactory. Therefore, the nominal diameter and pitch of the threaded portion of the rod should be 8mm and 1.25 mm respectively. Equating shear resistance of the threaded to the tension in the rod,  $\pi d_c l r = P$ ,  $\tau = 27$  N/mm<sup>2</sup>,  $\pi d_c l r = P$ ,  $\pi \times 6.466 \times l \times 27 = 400$   $l=0.73$  m,  $l=d=8mm$ ,  $l=1.25d=1.25 \times 8$ ,  $l=10mm$ , assumed as 9mm.

## 6. Design of Coupler

$D = 8.468 \text{ mm}$

Standard portion,  $D = d = 8$ ,  $D = 1.5d = 1.5 \times 8$ ,  $D = 12 \text{ m}$ , assumed as  $11 \text{ mm}$

**Check for Design**  $M_t = 313.6 \text{ N-mm} = D/2 = 12/2$ ,  $r = 6 \text{ mm}$ ,  $J = 1035.25 \text{ mm}^4$   $\tau = 1.66 \text{ N/mm}^2$

$\sigma_t = 8.935 \text{ N/mm}^2$ ,  $\sigma_{\text{max}} = 9.23 \text{ N/mm}^2$ , Factor of safety  $17.90$  is satisfactory, Now remaining dimension of turnbuckle.,  $D_1 = d + 10 = 8 + 10$   $D_1 = 18 \text{ mm}$ ,  $D_2 = 2 \times D_1 = 2 \times 18$   $D_2 = 36 \text{ mm}$ ,  $L = 6 \times d = 6 \times 8$ ,  $L = 48 \text{ mm}$

## 7. Design of Spring

Assume material: - SAE6145- oil quenched and drawn  $425^\circ\text{C}$ , From data book by B.D. Shiwalkar,  $S_{ut} = 1570 \text{ N/mm}^2$ ,  $G = 84 \times 10^3 \text{ N/mm}^2$

**Step 1:-** Wire diameter of spring Shear stress ( $\tau$ ) =  $0.5 \times S_{ut} = 0.5 \times 1570$ ,  $\tau = 785 \text{ N/mm}^2$ , Load ( $P$ ) =  $4 \text{ Kg} = 4 \times 9.81 = 39.24 \text{ N}$ , Wahl factor;  $K = 1.2525$ , Where,  $C = 6$  (standard value),  $d = 0.978 \text{ mm}$ , selected the wire diameter value as  $1 \text{ mm}$

**Step 2:-** Mean coil Diameter

$D = 5.868 \text{ mm}$ , So selecting safe value as  $D = 10 \text{ mm}$

**Step 3:-** No of active Coils

Assume deflection ( $\delta$ ) =  $150 \text{ mm}$  for load of  $4 \text{ kg}$  i.e.  $39.24 \text{ N}$ ,  $N = 40.23 \text{ turns} = 41 \text{ turns}$  Minimum safe number of turns occurring to be  $41 \text{ turns}$ . Hence, selecting  $N = 44 \text{ turns}$ .

**Step 4:-** Required spring rate  $k = 0.261 \text{ N/mm}$

**Step 5:-** Actual spring rate  $k = 0.243 \text{ N/mm}$ . Selecting the following design dimensions as  $d = 1 \text{ mm}$ ,  $D = 10 \text{ mm}$ ,  $N = 44 \text{ turns}$

## 8. Experimentations

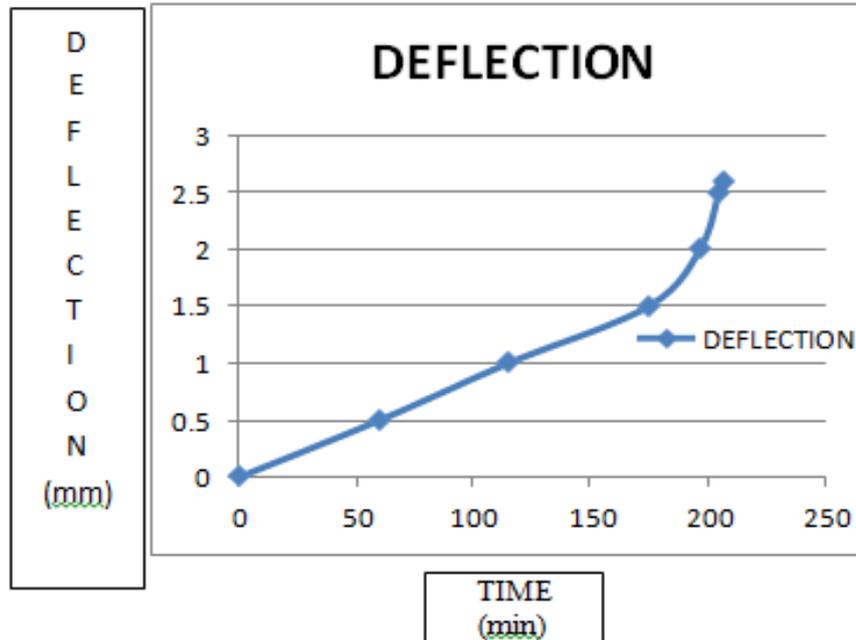
### 8.1. Experimentation-1

Material	Lead
Constant temperature	$70^\circ\text{C}$
Constant load	$3 \text{ kg}$
Time (min)	Deflection (mm)
0.00	-
60	0.5
115	1.0
17	1.5
197	2.0
205	2.5
207	2.6

**Table 2: Experimentation-1**



**Figure 3: Lead Sample, Expt.1**



**Graph 1: Deflection vs Time Graph**

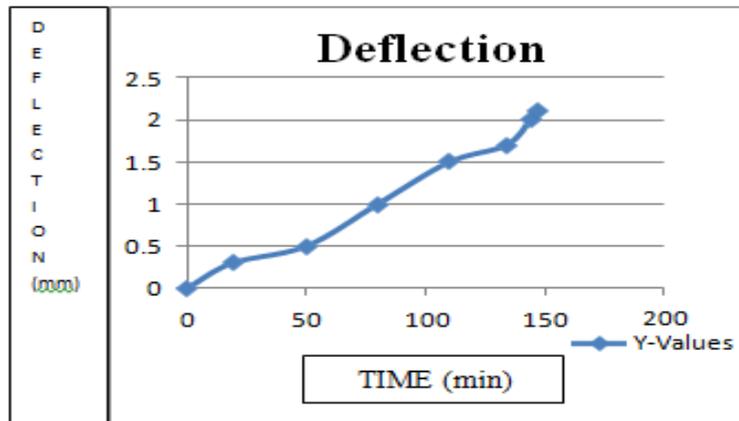
**8.2. Experimentation-2**

Material	Lead
Constant temperature	75°C
Constant load	2.5kg
Time(min)	Deflection(mm)
0	0
19	0.3
50	0.5
80	1
90	1.5
134	1.7
144	2
147	2.1

**Table 2: Experimentation-2**



**Figure 4: Lead Sample, Expt.2**



**Graph 2: Deflection vs Time Graph**



**Fig No. 5 Actual Experimental Setup**

## 9. Result and Discussion

Experimental creep test were performed on lead specimen with thickness of 1.5 mm and gauge length of 30 mm. In each experiment a constant temperature and load is maintained and creep behaviour is studied with respect to time. Deflection of Lead material at constant Load and Temperature

The purpose of this project was to design and fabricate a creep test apparatus which can be used in laboratory to demonstrate creep behaviour of engineering material without using expensive creep testing machine. Turnbuckle of stainless steel having  $S_{ut} = 465$  MPa and  $S_{yt} = 270$  MPa, M8 designated was selected according to design calculation and a tensile spring SAE6145- oil quenched drawn 425°C having  $S_{ut} = 1570$  N/mm<sup>2</sup> and shear modulus of  $84 \times 10^3$  N/mm<sup>2</sup> were selected according to design calculations

## 10. Future Scope of Action

Analysis work using different materials can be carried out by using the machine. By adding more electronic component like extensometer and data acquisition system, etc., the machine can be made fully automatic and more accurate analysis can be done.

## 11. References

1. Kenneth Kanayo Alaneme, Bethel Jeremiah Bamike, Godwin Omlenyi, "Design and Performance Evaluation of a Sustained Load Dual Grip Creep Testing Machine", Journal of Minerals and Materials Characterization and Engineering, Vol. 2, Issue 2, Page 531-538, 2014.
2. Muhammad Zubair Khan , Hassan Saleem, Adil Mahil , Aleemullah, Fazal Ahmed Khalid ,Syed Asad Ali Naqvi, Tak-Hyoung Lim, Rak- Hyun Song, "Design and Fabrication of High Temperature Creep Testing Machine", American Journal of Materials Engineering and Technology, Vol. 3, Issue 3, Page 51-57, 2015.
3. J. L. Chukwunke1, P. C. Okolie1 , D. C. Ugwuegbu2 and J. E. Sinebe3, "Design Analysis and Fabrication of a Tensile Creep Testing Machine", British journal of applied sciences and technology, Vol.14, Issue3, Page 1-13, 2016.
4. Salah K. Jawad, Investigation of the Dimensions "Design Components for the Rectangular Indirect Resistance Electrical Furnaces", American Journal of Engineering and Applied Sciences, Vol. 3 Issue2, Page 350-354, 2010.

5. M Scibetta , A. Pellettieri, P. Wouters, A. Leenaerts, G. Verpoucke, “Design and Fabrication of a Dead Weight Equipment to Perform Creep Measurements on Highly Irradiated Beryllium Specimens”, in Proc. HOTLAB Plenary Meeting ( Halden, Norway, Sept.2004) pp.-142
6. Jan Kolarika,, Alessandro Pegoretib, “Non-linear tensile creep of polypropylene: Time-strain superposition and creep predictions Engineering and Industrial Technologies” ,Polymer, Vol. 47 Pages 346–356, 2006
7. Jonathon Tanks, Katherine Rader, Stephen Sharp, Takenobu Sakai, “Accelerated creep and creep-rupture testing of transverse unidirectional carbon/epoxy lamina based on the stepped isostress method”, Composite structures Charlottesville, Vol.159, Pages 455-465, 2017.
8. Rongguo Zhao, Chaozhong Chena, QifuLia, Xiyan Luoa , “Accelerated characterization for long-term creep behavior of polymer” in Proc. International Conference on Experimental Mechanics · (china,Nov.2008)pp.-73751D-1-73751D-6
9. McDanel, D. L., “Analysis of stress-strain, fracture and ductility behaviour of aluminium matrix composites containing discontinuous SiC reinforcement”. Metall. Trans. A, Vol.16, Pages1105-1115,1985
10. B. Ralph, H.C. Yuen and W.B. Lee, “The processing of metal matrix composites — an overview”, Journal of Materials Processing Technology, Vol. 63, Issue 1-3, Pages 339-353, 1997
11. S.V.S. Narayana Murty, B. Nageswara Rao, B.P. Kashyap, “On the hot working characteristics of 6061Al–SiC and 6061–Al<sub>2</sub>O<sub>3</sub> particulate reinforced metal matrix composites, Composites science and technology Vol.63, Pages 119-135,2003
12. Barbara Previtali, Dante Pocci , Cataldo Taccardo,” Application of traditional investment casting process to aluminium matrix composites, Composites: Part A, Vol. 39,Issue 1-2, Pages1606- 1617,2008